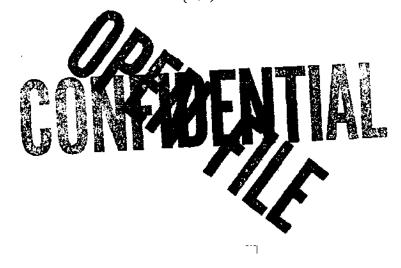
PR. BULLMOOSE TR(1)A.



REPORT ON BULLMOOSE PROJECT, 1972 SUKUNKA RIVER AREA, B. C.

by

· R. S. Verzosa

January 30, 1973 Vancouver, B.C.

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TABLE OF CONTENTS

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	Page
INTRODUCTION	1
SUMMARY AND CONCLUSIONS	2
GENERAL GEOLOGY	2
Geologic Setting	2&3
STRATIGRA PHY	3
Bullhead Group Cadomin Formation Gething Formation	3 3 3 & 4
Fort St. John Group Moosebar Formation Commotion Formation	5 5 5
Sukunka Member Gates Member Hulcross Member Boulder Creek Member	5&6 6 6&7 7
Hasler Formation	7
STRUCTURE	8
Folds	8
Faults	8 & 9
COAL SEAMS	9 & 10
Chamberlain Seam Skeeter Seam Bird Seam Coal Seam Intersections - Upper Gething	10 11 11 11
Sample Analysis	11 & 12
DIAMOND DRILLING	12 & 13
STATEMENT OF EXPENDITURES	14

A PPENDIX ICoal Sample Analyses SEE: PR-BULINGOSAttached
72 (A)AAPPENDIX IIExploration Report by R. E. Hindson-Separate Cover

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SHORT LIST OF ILLUSTRATIONS

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Figure 1	Property Location Map	after page 1
Figure 2	Stratigraphic & Correlation Chart	after page 3
Plate 1	Geologic Map, 1" = 1000'	Pocket
Plates 2,3,4,5	Columnar Sections of T-16, T-17, T-18, T-19	Pocket
Plates 6,7,8,9	Gamma ray-Neutron and Sidewall Density logs of T-16 and T-19	Pocket
Plate 10	Cross Section along line A	Pocket
Plate 11	Cross Section along line 6	Pocket

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INTRODUCTION

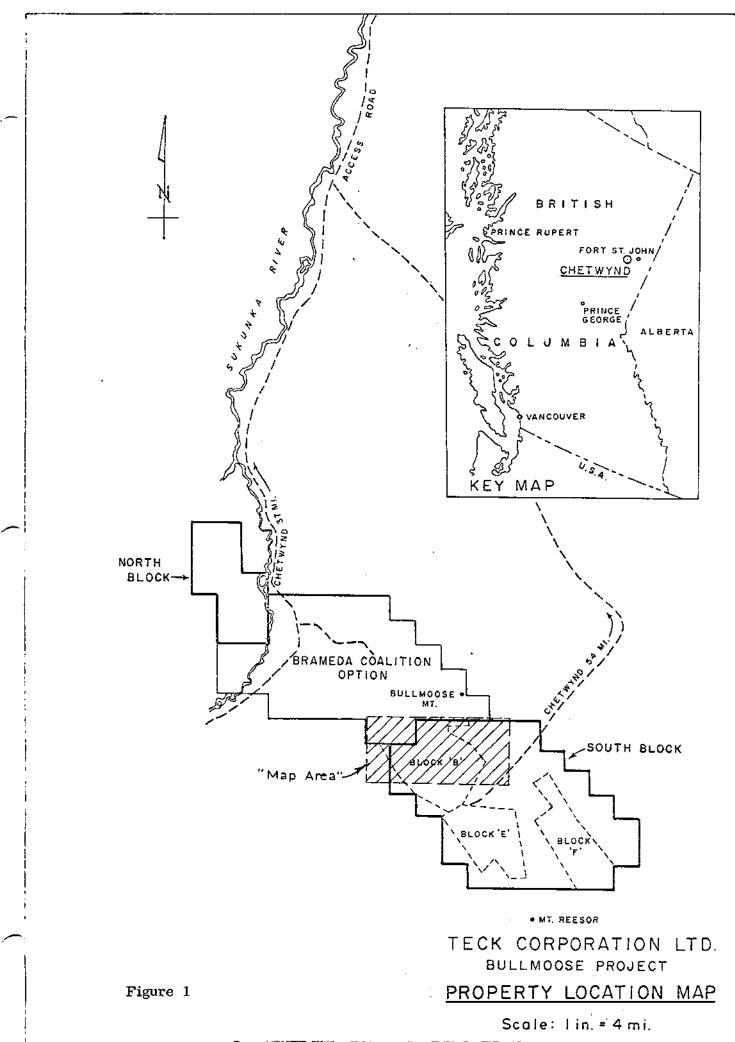
This report contains details of work done in 1972 by Teck Corporation Limited on a block of ground covering a number of coal licences in the Sukunka River area, British Columbia (Figure 1). The area is located southeast of Chetwynd, British Columbia and is accessible through 48 miles of gravel road.

The work completed in 1972 primarily consisted of diamond drilling and geologic mapping in a limited programme that was essentially a part of a continuing effort by Teck Corporation Limited to evaluate the coal potential of the area. The drilling totalled 3,692 feet in 4 holes that were spaced 2000 feet from previously drilled holes.

In 1971 Teck Corporation Limited carried out an extensive drilling and geologic mapping programme in two areas designated as Block "B" and Block "E" (Figure 1). That programme resulted in the completion of a comprehensive geologic map of the important part of the area and of a total of 14,657 feet of drilling in 15 holes.

For purposes of this report the section on Geology is presented only as a summary of the general geology of the area. A detailed account of the geology of the area is contained in a report by R. E. Hindson, 1972, entitled "Exploration Report, Teck Corporation Limited" a copy of which is appended herein.

The term "map area" used in this report refers to the area covered by the enclosed geologic map covering a northwestern portion of the property.



SUMMARY AND CONCLUSIONS

- 2 -

The Teck property in the Sukunka River area is underlain by Lower Cretaceous sediments belonging to the Bullhead and Fort St. John Groups and includes the coal-bearing Gething Formation. The sediments are generally less deformed, the prospective part of the area being on a gently dipping limb of a broad syncline.

The outstanding Chamberlain seam that is presently being developed by Coalition Mining Ltd. to the north continues southward into the property although a sedimentary facies change within the seam drastically diminishes its thickness and quality as it progresses further south. The Skeeter seam is consistently represented in most of the drill holes and closely ranks with the Chamberlain seam in quality but does not show sufficient thickness to warrant further appraisal. The Bird seam exhibits a consistent thickness of greater than 6 feet over a wide area but the seam contains an exceedingly high sulfur. This undesirable feature coupled with the fact that the seam is practically roofed by the incompetent Moosebar Formation makes an economic evaluation of the seam impractical at the present time.

Additional drilling is required to further evaluate the Chamberlain seam in the Teck property particularly in regard to the limiting effect of the facies change within the seam on the coal potential of the property. The area bounded by the prominent synclinal axis to the west, the Coalition property line to the north and the latitude of T-8 to the south offers good prospecting ground.

GENERAL GEOLOGY

Geologic Setting

The immediate area is underlain by a sequence of marine and nonmarine clastic rocks belonging to the Lower Cretaceous Bullhead and Fort St. John Groups of the Peace River area. It lies in a northwesterly belt that is relatively undeformed and is bounded to the west and east by similar tightly folded and thrust-faulted strata.

STRATIGRA PHY

The stratigraphy of the map area in this report is based on rock exposures along Saddle Creek, drill cores of T-19 and outcrops along the cirque west of base camp No. 1. Nomenclatures are adopted from Stott (1968) and correlations are made solely on lithologic characteristics. No detailed stratigraphy is available of the Lower Gething due to the lack of continuous exposures. However, detailed stratigraphic descriptions of the Upper Gething up to parts of the Gates Member of the Commotion Formation are contained in columnar sections of diamond drill holes.

Bullhead Group

Cadomin Formation

The cliff-forming conglomerate along Saddle Creek consists of granules to rounded pebbles and cobbles of quartz, chert and metasediments in a very coarse quartzose sandstone matrix. The phenoclasts are generally poorly sorted and the formation as a whole contain inter-tongues of cross-bedded very coarse massive sandstone. Although the base of the formation was not directly observed the Cadomin in Saddle Creek is at least 300 feet thick. The Cadomin is conformably overlain by the Gething Formation.

Gething Formation

In the map area the coal-bearing Gething Formation is sub-divided into two members, vis. the Upper Gething and the Lower Gething. Although there is essentially no formational change from one member to another a distinct recognition of the Chamberlain coal seam makes the sub-division not

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STRATIGRAPHIC AND CORRELATION CHART

	Τc	ck Area (1973)) [Stott (1968)	Teck Area
Group		Formation	Thickness Feet		Formation	Thickness Feet	Lithology
		Hasler	450		llasler	500?-1500	Dark grey interbedded shale, siltstone and mudstone with ferruginous concretions and layers. Local minor conglomerate.
e		Boulder Creek Mb	300		Boulder Creek Mb	240 - 560	Fine to medium-grained sandstone; interbedded siltstone and mudstone, in parts conglomeration
. John	£	Hulcross Member	300	otion	Hulcross Member	0 - 450	Dark grey marine shale and mudstone with common pyritic and ferruginous concretions.
S S	MemberMemberCommon pyritic and ferruginous conciGates920Gates220 - 900Fine to medium to coarse sandstone with pyritic and siltGates920MemberMemberCoal. Layers of massive pebble congSukunka430Moosebar100 - 1000Interbedded fine-grained sandstone, and siltstone.MemberNoosebar100 - 1000Dark grey mudstone with pyritic and	Fine to medium to coarse sandstone with interbedded shale, mudstone and siltstone. Coal. Layers of massive pebble conglomerate.					
	U U		430		Nooschar	100 - 1000	
Sukunka 430 Interbedded fine-grained sandston Member Noosebar 100 - 1000 and siltstone. Dark grey mudstone with pyritic and siltstone Dark grey mudstone with pyritic and siltstone	Dark grey mudstone with pyritic and ferruginous concretions and lavers						
	ng.	Upper	113-205		Cathian	75 1000	Fine to medium to coarse-grained sandstone with interbedded shale, mudstone and siltstone Chamberlain Seam at base. Glauconitic mudstone at top.
Bullhead	Gethiı	Lower	1200		Getating	15 - 1000	Fine to medium to coarse-grained sandstone with interbedded shale, mudstone and siltstone Locally carbonaceous. Coal and coaly seams near base. Local thin conglomerates.
Bu	Beulder Creek Mb300Boulder Creek Mb240 - 560Fine to medium-grained sandstone; interbed siltstone and mudstone. in parts conglomer siltstone and mudstone. in parts conglomer Dark grey marine shale and mudstone with common pyritic and ferruginous concretions of acesGates Member92090Gates Member220 - 900Fine to medium to coarse sandstone with interbedded shale, mudstone and siltstone Coal. Layers of massive pebble conglomer and siltstone. Dark grey mudstone with pyritic and ferruginous concretions and layersSukunka Moosebar430Moosebar100 - 1000Interbedded fine-grained sandstone, mudstone and siltstone. Dark grey mudstone with pyritic and ferruginous concretions and layersUpper113-205Gething75 - 1000Fine to medium to coarse-grained sandstone with interbedded shale, mudstone and siltstone .Example1200Gething75 - 1000Fine to medium to coarse-grained sandstone with interbedded shale, mudstone and siltstone .						

Figure 2. Stratigraphic and Correlation Chart of the Lower Cretaceous in the Teck Bullmoose Project area.

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only possible but for mapping purposes convenient.

- 4 -

The Lower Gething exposed along Saddle Creek consists of a sequence of medium-bedded to massive, medium to coarse to very coarse sandstone with interbedded siltstone, mudstone and shales. Occasional to common occurrences of carbonaceous and coaly partings are found throughout the section. At a point approximately 350 feet stratigraphically above the top of the underlying Cadomin Formation is a 20 foot interlaminations of carbonaceous siltstone and mudstone with coal partings and bands of up to 1 inch thickness at its base. A 2 foot coal seam is present approximately 50 feet stratigraphically above the top of the Cadomin. The thickness of the Lower Gething measured from the top of the Cadomin to the base of the Chamberlain seam as exposed along Saddle Creek is approximately 1200 feet.

The Upper Gething in the map area consists of flaggy, fine to medium to coarse grained, medium to thick-bedded sandstone in its upper half and interbedded to interlaminated fine sandstone, siltstone and mudstone in its lower half. The unit contains the Bird coal seam near its top and the Skeeter and Chamberlain coal seams at its base. Overlying the Bird seam is a thin but persistent layer of glauconitic and commonly pyritic argillaceous and occasionally pebbly sandstone which serves as a marker between the Gething Formation and the overlying Moosebar Formation.

The nature of the contact between the Upper Gething and the overlying Moosebar Formation is not clear although the indicated difference in the sedimentary environments between the two may suggest at least a disconformable relationship. The thickness of the Upper Gething as shown by drill holes in the map area taken from the base of the overlying Moosebar Formation to the base of the Chamberlain seam is variable and range from 113 feet in DDH T-7 to 205 feet in DDH T-19. The variations in thicknesses could partly be due to repetition of strata by faulting.

Fort St. John Group

Moosebar Formation

The Moosebar Formation overlying the Gething primarily consists of a dark brown to dark grey brittle mudstone. A number of sideritic and bentonitic layers may abound anywhere within the section although the bentonitic layers usually occupy the lower half. Pyrite nodules and concretions are common towards the base of the section. The only criteria for recognition of the Moosebar is its stratigraphic position in relation to the underlying Gething and the overlying Commotion Formation. Lithologically it is similar to some mudstone horizons within the Gething and to some parts of the Hulcross Member of the Commotion Formation. The Moosebar Formation grades insensibly into the overlying Sukunka Member of the Commotion although for purposes of mapping its upper contact is arbitrarily set at the first appearance of a sandstone layer of the overlying Sukunka Member. The thickness of the Moosebar Formation gathered from drill hole data in the area show an approximate average of 300 feet.

Commotion Formation

Sukunka Member:

The term "Sukunka" is the result of the study of previous workers on the Brameda-Coalition ground immediately north of the map area. The member is equivalent to the upper part of the Moosebar Formation described by Stott in his study of the Peace River area. In the map area the Sukunka Member consists of a sequence of interbedded to interlaminated sandstone, siltstone and mudstone. The sandstone and siltstone units are generally cross-bedded and ripple marked and occasionally contain plant fossils and/or carbonaceous partings. The sandstone increases in proportion upwards and at the same time

gets coarser-grained. In the map area the upper contact of the Sukunka Member is set at the base of the massive coarse-grained sandstone below the lowest conglomerate horizon of the conformably overlying Gates Member. Its thickness from drill hole data in the map area show an average of 430 feet.

Gates Member

The prominant ledges, cliffs and cirques on the eastern part of the map area is formed by the coarse sandstone and conglomerate units of the Gates Member. Interbedded with the sandstone and conglomerate are finer clastics of generally carbonaceous shale, siltstone and mudstone. In the middle part of the section, particularly in DDH T-19 at least six coal seams are present ranging in thickness from 6 inches to as much as 3-1/2 feet.

The conglomerate units in the Gates consists of well sorted, subrounded to rounded granules and pebbles of quartz and chert in a medium to coarsegrained quartzose sandstone matrix. The outcrops are generally massive and very thick-bedded. The upper contact of the Gates Member with the overlying Hulcross Member in the map area lies on top of a thin layer of conglomeratic sandstone and is well observed in cores of previous diamond drilling. The contact is sharply defined and exactly conforms with Stott's (1968) description of the Hulcross Member at its type locality. The thickness of the Gates Member in the map area is approximately 920 feet.

Hulcross Member:

The Hulcross Member in the map area is exposed along the cirque west of Base Camp No. 1 and along a number of access roads in the property. On outcrops the Hulcross comprises an interbedded sequence of generally dark brown to dark grey fine sandstone, shale, siltstone and mudstone. Ferruginous

layers and concretions are variably common and imparts a bright reddish brown colour to some weathered outcrops that usually can be seen from a distance. Although the upper contact of the Hulcross Member was not physically observed by the writer it reportedly grades into the sandstones of the overlying Boulder Creek Member. The mapped thickness of the Hulcross Member southeast of Base Camp No. 1 is at least 300 feet.

Boulder Creek Member:

The elevated area bordered by sheer drops and hogbacks in the west central part of the map area is underlain by predominantly thick-bedded conglomeratic sandstone of the Boulder Creek Member. This member is described in detail by Stott (1968) and Hindson (1972) and reportedly includes three consistent facies; a lower, consisting of bedded, fine-grained sandstone; a middle, consisting of a massive conglomerate; and an upper, consisting of sandstone, siltstone, mudstone and coal. Immediately west of Camp No. 1 in the property the cliffs are formed by granular to pebbly to conglomeratic, fine to very coarse, cross-bedded and thick-bedded to massive quartzose sandstone. Occasionally along the section are interbeds of thin dark brown siltstone and mudstone. The top of the Boulder Creek Member in the map area was not observed although a minimum of 300 feet of thickness is indicated.

Hasler Formation

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The Hasler Formation occupies the top of the stratigraphic sequence in the property. The formation was not observed by the writer although it was recognized and magned by Hindson for Took in 1971. The Hasler Formation theastrop Mount chamberlain and reportedly occurs in an crossional remnant sou itstone and within the section minor consists of interbedded shale and s ness measurement was reported although conglomeratic sandstone. No thick in the map.

- 7 -

STRUCTURE

Folds

The dominant structural trend in the map area is north-northwest with bedding attitudes ranging from zero to a maximum of 75 degrees. In the central part of the map lies a broad assymetrical syncline whose eastern limb dips a gentle 15 degrees. Its western limb dips as much as 75 degrees and forms the eastern limb of a tightly folded northwesterly anticline whose axis lies only a few hundred west of Mount Chamberlain. Other less significant folds were mapped along the slope north of Saddle Creek.

The majority of bedding attitudes measured from drill cores average 5 to 12 degree dips. However, higher dips of 25 degrees and as much as 60 degrees were recorded in strata close to or within the coal seams in the Upper Gething. These higher dips are limited and are believed to have been localized by the less competent coal seams.

Faults

Other than a thrust fault that separates the Sukunka Member and the Lower Gething on the southwest corner of the map area no other fault of signifcant magnitude is known. Along Saddle Creek a northerly thrust fault dipping 28 degrees west was noted and local marker planes indicate a vertical displacement of not more than 20 feet. The tightly folded anticline west of Mount Chamberlain is breached by a minor northwesterly high angle thrust fault dipping 70 degrees west with a vertical displacement of only about 15 feet. From drill core observations particularly in the Moosebar Formation a number of faults evidenced by crushed zones, gouge and slickensides were noted. However, the lack of marker beds in the Moosebar Formation prevents the measurement of vertical displacement along these fault planes, but judging from the fairly consistent thickness of the Moosebar formation from one hole to another the vertical displacements that could result from these number of

faults are probably minor in regard to their significance to the underlying coal seams. Furthermore, the incompetence of the Moosebar Formation could have confined these structural features within itself so as not to be appreciably reflected by the overlying and underlying strata. Additional drilling could provide information leading to a more reliable interpretation of the subsurface structure of the area.

COAL SEAMS .

The main target of exploration in the property is the so-called Chamberlain seam which in the Brameda-Coalition option immediately to the north has been recognized and verified to be consistently high in quality with indicated reserves exceeding 60 million tons.

While a number of other seams exist in the Teck property particularly those in the Gates Member of the Commotion Formation and in the Lower Gething Member only the important Bird, Skeeter and Chamberlain seams that are found in the Upper Gething are considered and described in this report. Drill logs from previous drilling have been referred to in assessing the general character of each individual seam.

Coal outcrops in the area are generally poor except where found in deeply incised gullies. On one of the northerly tributaries of Saddle Creek both the Chamberlain and Skeeter seams are well exposed. Another small tributary in the same vicinity offered an excellent exposure of the Bird seam. However, the massive and hard sandstone layer that forms the floor of the Bird and Chamberlain seams is easily recognizable and stand out as ledges along steeper topographies. On top of these sandstone ledges and under 6 to 12 inches of top soil weathered coal mixed with overburden can usually be found thus, providing a means for mapping. Because of the general lack of good

- 9 -

exposures the descriptions of the coal seams that follow are primarily based on diamond drill intersections.

Chamberlain Seam

The Chamberlain seam is characteristically hard and exhibits alternating bands of bright and dull coal. The seam rests on a massive coarse-grained carbonaceous sandstone floor and is generally roofed by thin bedded and interbedded commonly carbonaceous siltstone and shale. The seam thickness vary although at least five drill holes including 2 holes drilled in 1971 returned a minimum thickness of 12 feet. The general character of the seam changes to the south and southwest and takes one or a combination of forms such as thinning, splitting into as much as 5 seams and/or exhibits varying amounts of clastic components within the seams such as sandstone and shale. No study has yet been made to determine the character of the facies changes within the seam in the area insofar as its economic implication is concerned. Additional drilling would be required to provide a reliable picture in this regard.

Skeeter Seam

The Skeeter seam is generally less harder than the Chamberlain seam and is usually duller in appearance. The seam is commonly roofed by carbonaceous sandstone that usually contains coal partings and wisps. The floor of the seam is about 20 feet above the roof of the Chamberlain seam and consists of interbedded sandstone, siltstone and shale. The thickness of the Skeeter seam ranges from less than 2 feet to less than 5 feet. The seam, like the Chamberlain seam below exhibits lateral facies changes southwestward.

Bird Seam

The Bird seam is hard and banded although generally dull. Pyrite disseminations and nodules are common to abundant particularly in the upper half of the seam. The Bird seam is roofed by the thin layer of glauconitic, and pyritic sandy mudstone or argillaceous sandstone that marks the top of the Gething Formation and rests on a massive coarse-grained carbonaceous sandstone. The thickness of the seam is fairly consistent over a wide area and averages only slightly more than 6 feet.

Coal Seam Intersections (Upper Gething)

All the four holes drilled in 1972 intersected the Bird, Skeeter and Chamberlain seams as follows:

Hole No.	Bird Seam	Skeeter Seam	Chamberlain Seam
T -1 6	1052.6-1071.5 1074.0-1077.5	1188.8-1193.5	1213.0-1214.5 1216.6-1238.5 1247.5-1265.1
T -17	248.0- 255.0 257.6- 258.6	342.0- 345.0	353.4- 357.8
T-1 8	337.0- 344.4	426.2- 429.6	454.0- 467.7
T-19	1366.0-1370.0 1371.0-1376.5	1462.0-1468.8	1488.0-1501.8

Sample Analysis

The Chamberlain seam intersected in holes T-16, T-17 and T-19 were sampled and designated as follows:

T-16	Sample 1	(1248.5 - 1258.0)	-	6" shale at base
	Sample 2	(1258.0 - 1261.1)	-	
T-17	Sample 3	(346.0- 353.4)	-	only 1.7' recovered
	Sample 4	(353.4- 357.8)		
T -1 9	Sample 5	(1488.0-1491.8)	-	1" shale at base
	Sample 6	(1491.8-1501.4)		

The cores of the Chamberlain seam in T-18 was not sampled and is being saved for future reference. The sampled cores were submitted to Commercial Testing and Engineering Company of North Vancouver for a standard coal analysis the results of which are appended in this report.

DIAMOND DRILLING

A total of 3,692 feet of NQ size diamond drilling in four holes was done by Connors Drilling Ltd. Only one drill rig was used and worked on a two-10 hour shift basis. No major delay was encountered during the drilling while 100 feet of drilling per shift was average under normal conditions.

Footage Distribution

Hole No.		Depth	Dip Angle
T-16		1,278'	-90 ⁰
T-17		408'	-900
T-1 8		. 488'	-90 ⁰
T-1 9		1,518'	-90 ⁰
	Total	3,692'	

Tropari Survey

As an adjunct to the diamond drilling operations at least one Tropari test was made in each hole. No more than 6 degrees deviation from vertical was recorded.

Bulldozer

A Caterpillar D-6C was made available during the entire drilling operations. Operating time mostly involved road repair, road building, drillsite preparation and moving the drill rig and equipment as required.

Borehole Logging

In this programme the use of gamma ray-neutron and sidewall density hole surveys was introduced for the first time on the property. Unfortunately, the equipment was not immediately available upon the completion of T-17 and T-18 where subsequent caving and bridging in the holes prevented the entry of the survey tool. As can be seen from the enclosed logs of T-16 and T-19 the important horizons within the formations as well as the widths of the individual coal beds are very well depicted. The logs of T-16 particularly confirms two coal beds comprising the Chamberlain seam and negates a previous interpretation that the two beds represented a repetition by faulting. Such borehole data could have resolved the problem of the Skeeter-Chamberlain seam intersection in T-17 where excessive core loss was encountered.

Respectfully submitted,

R. S. Verzosa, P. Eng.

January 29, 1973 Vancouver, B. C.

TECK CORPORATION LIMITED

"Bullmoose" Project Expenditures

From January 1, 1972 to September 30, 1972

Field Supervision, Engineering, and Administration	\$ 17,908.38
Geological Mapping	9,132.38
Diamond Drilling	33,646.41
Road Construction	5,839.98
Vehicle operation, travel, and transportation	2,687.12
Assaying	2,954.70
Camp Operation	620.47
Maps and prints	1,074.25
Telephone	24.45
General expenses	80, 36
Government licenses and fees	 2,872.65

\$ 76,841.15

Controller Teck Corporation Limited

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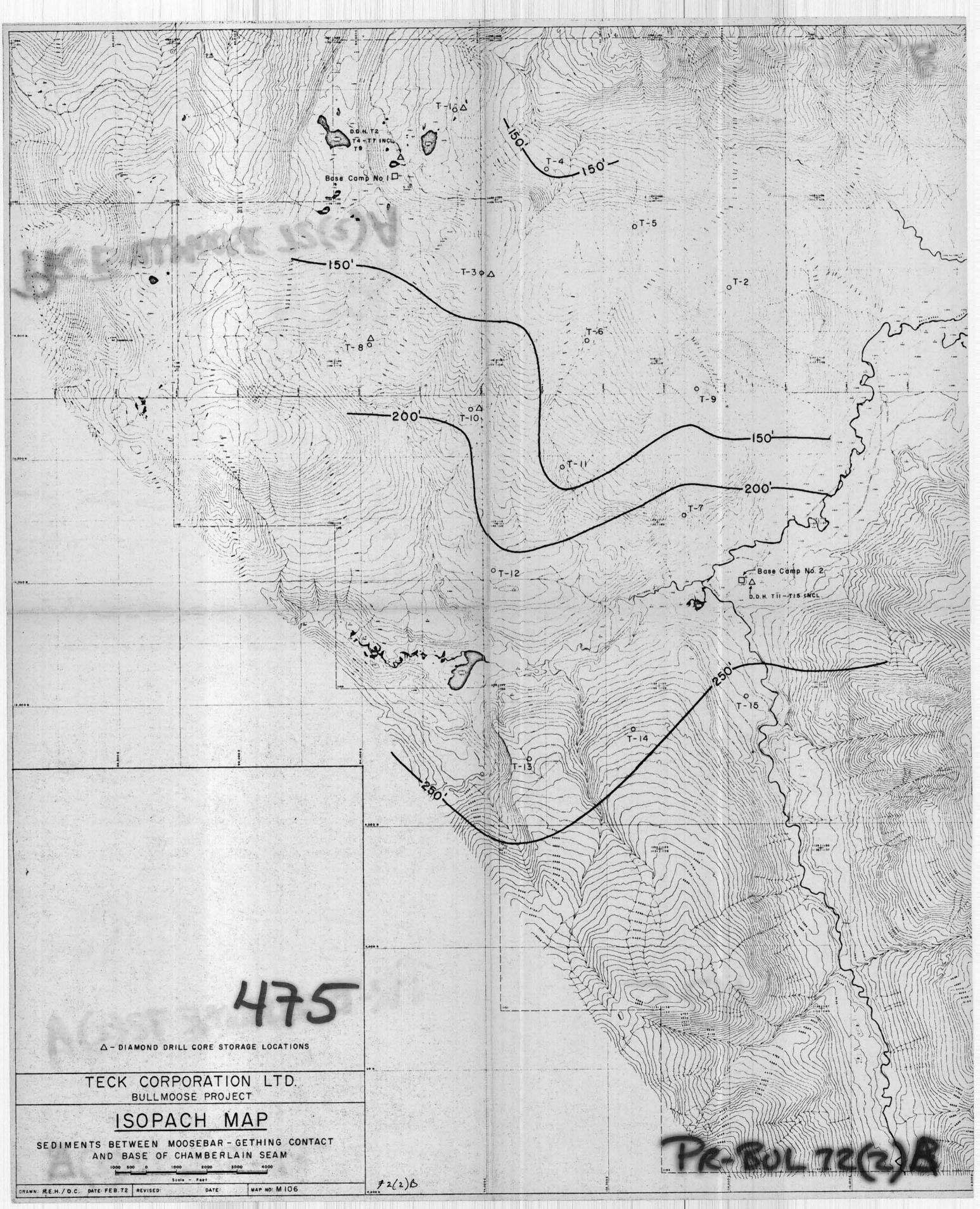
APPENDIX I : COAL SAMPLE ANALYSES

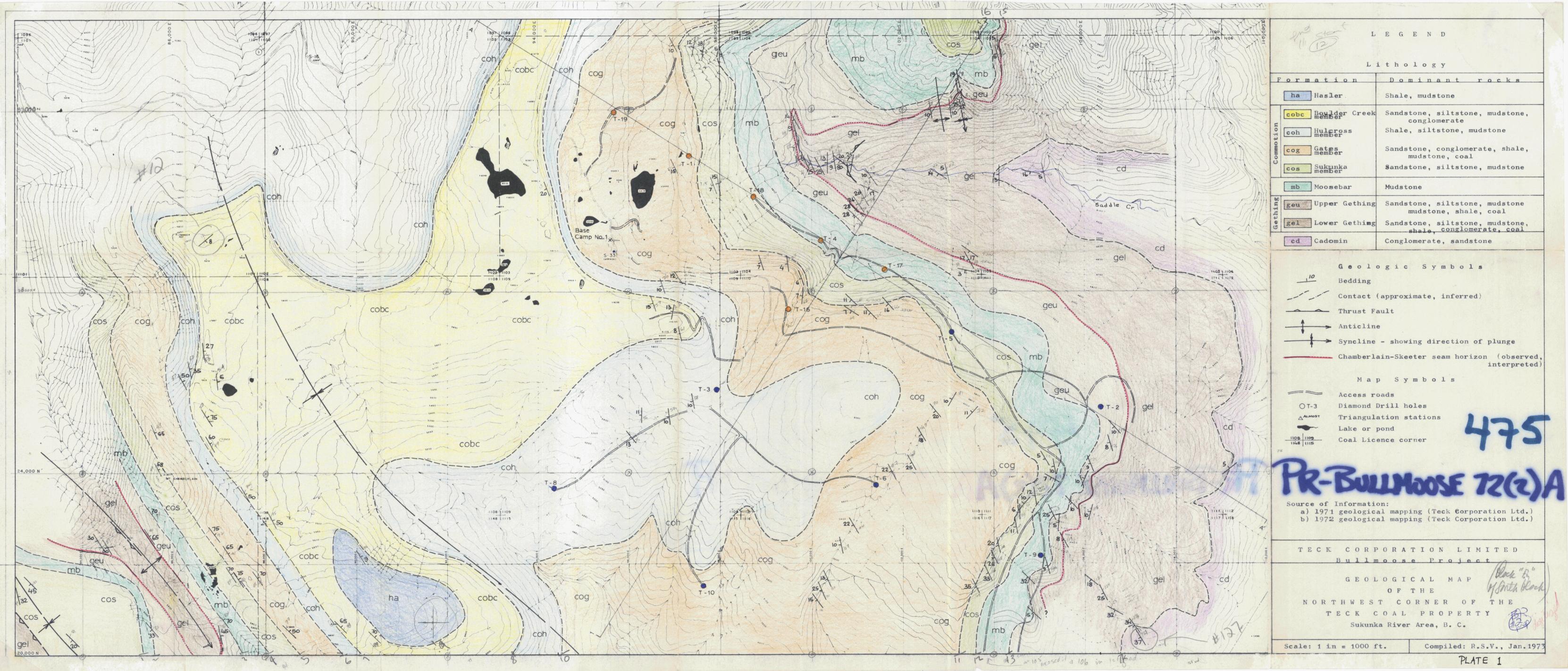
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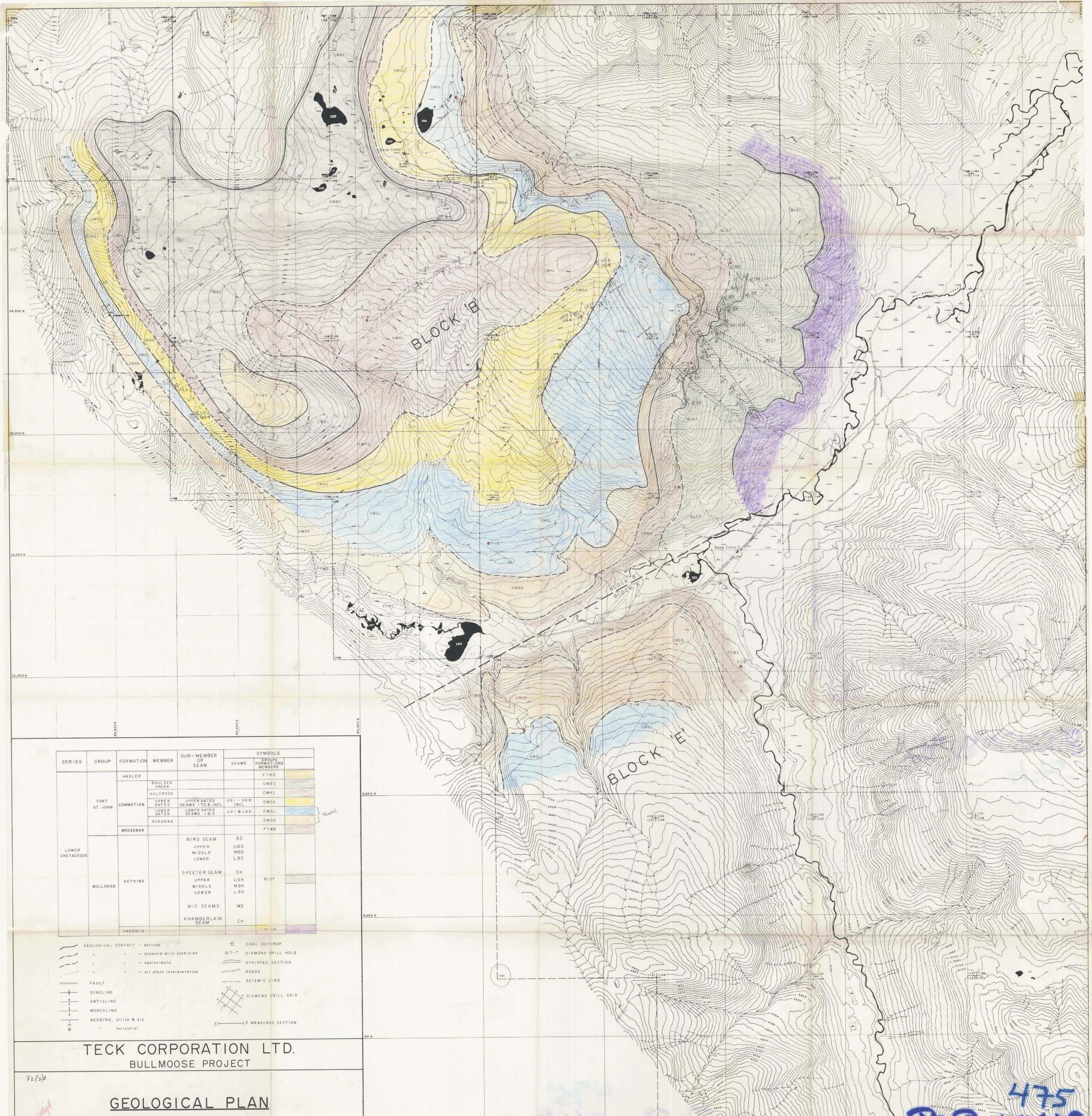
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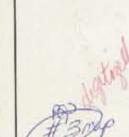
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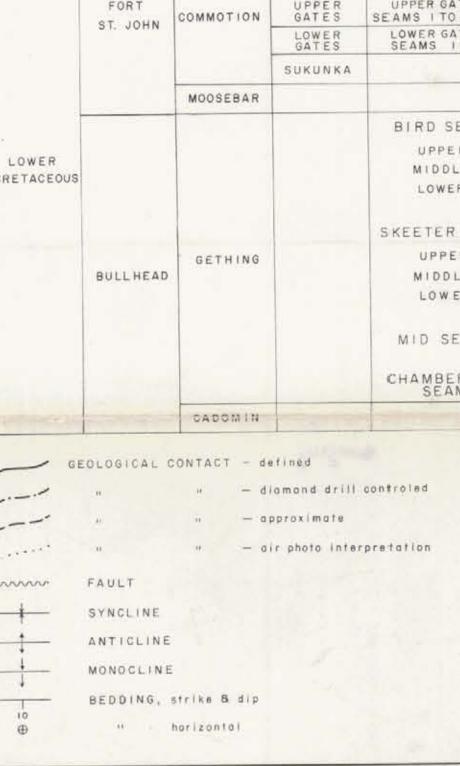
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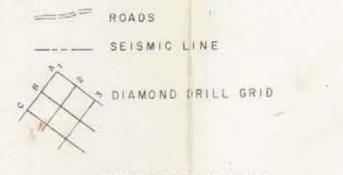








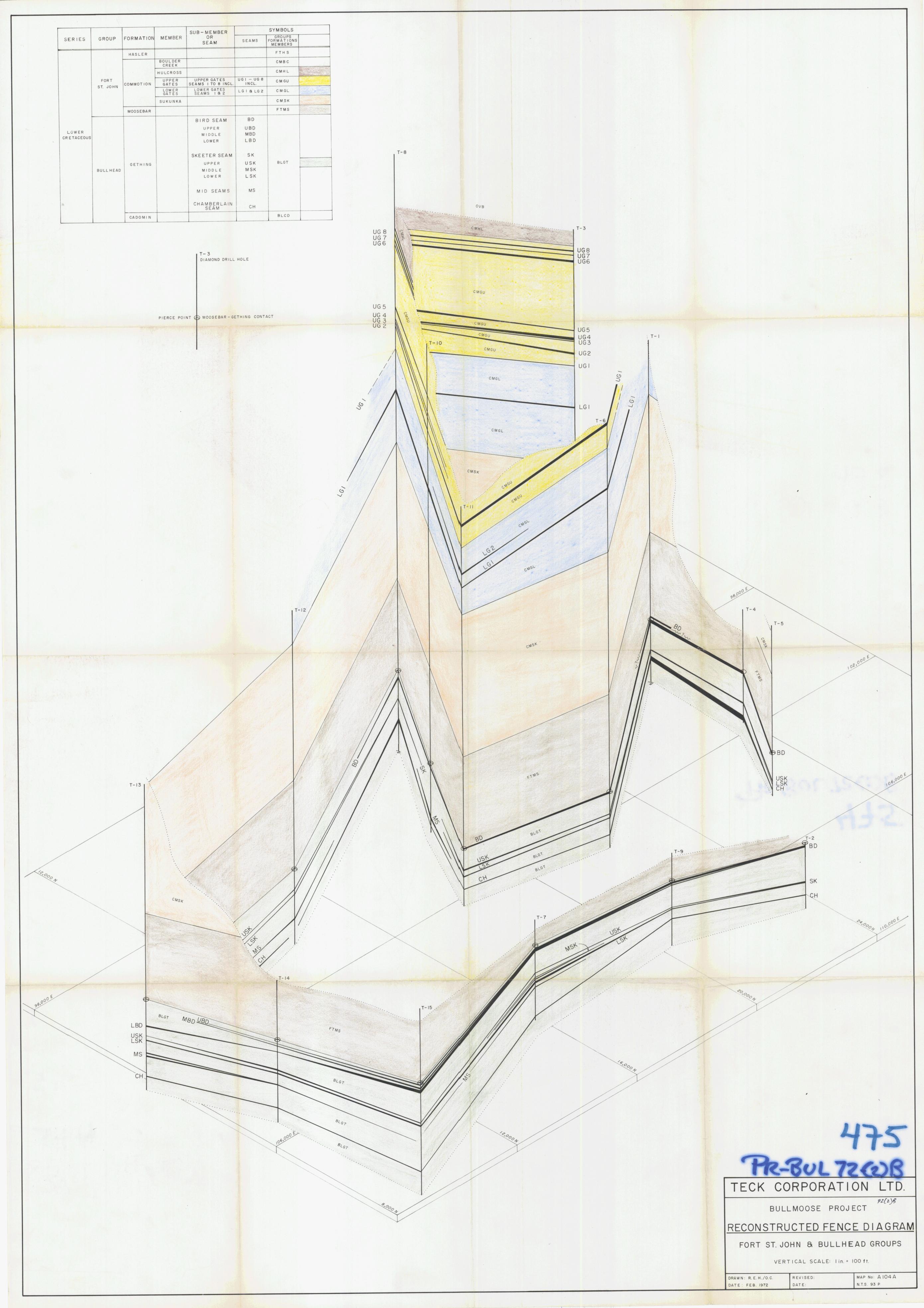


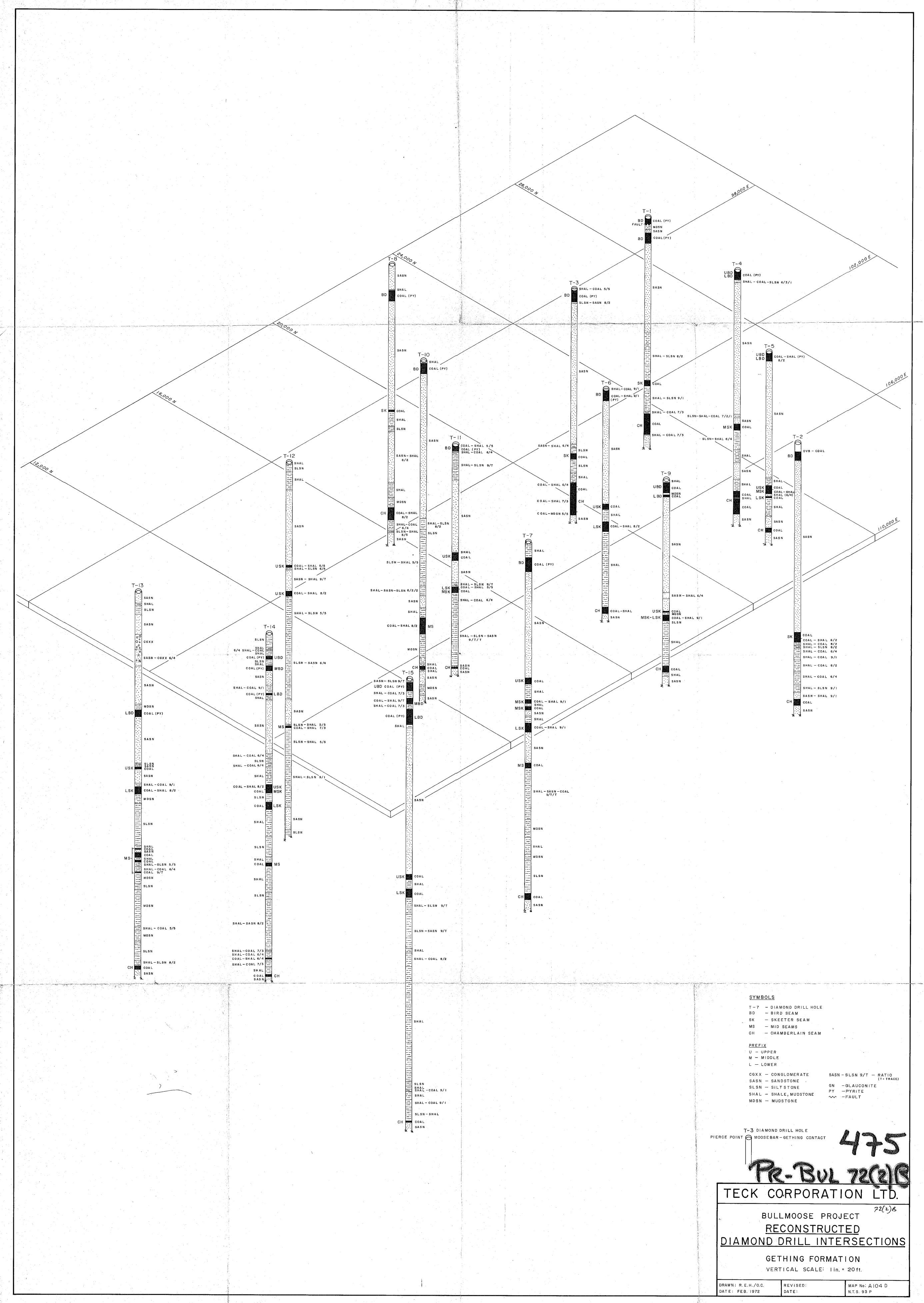


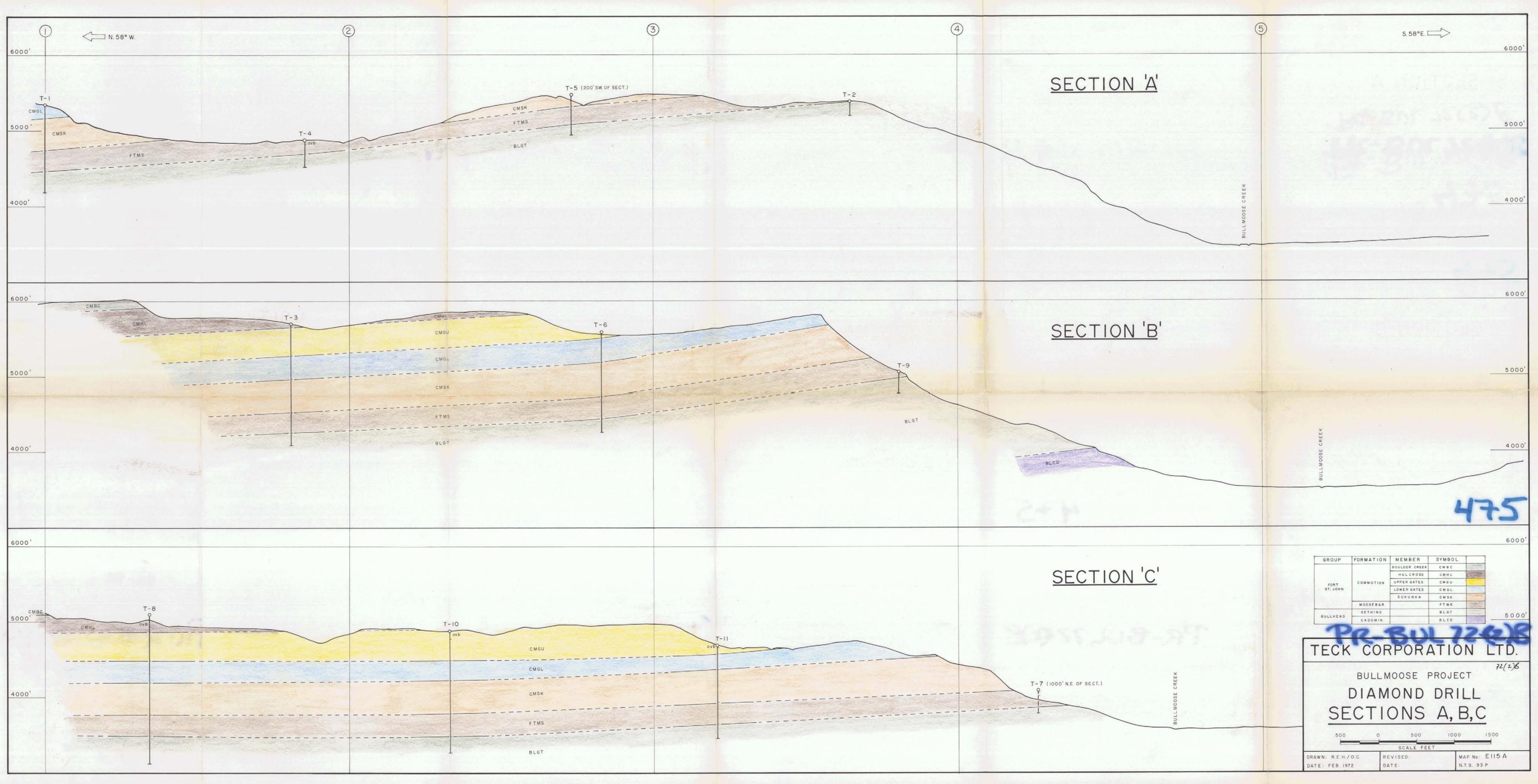
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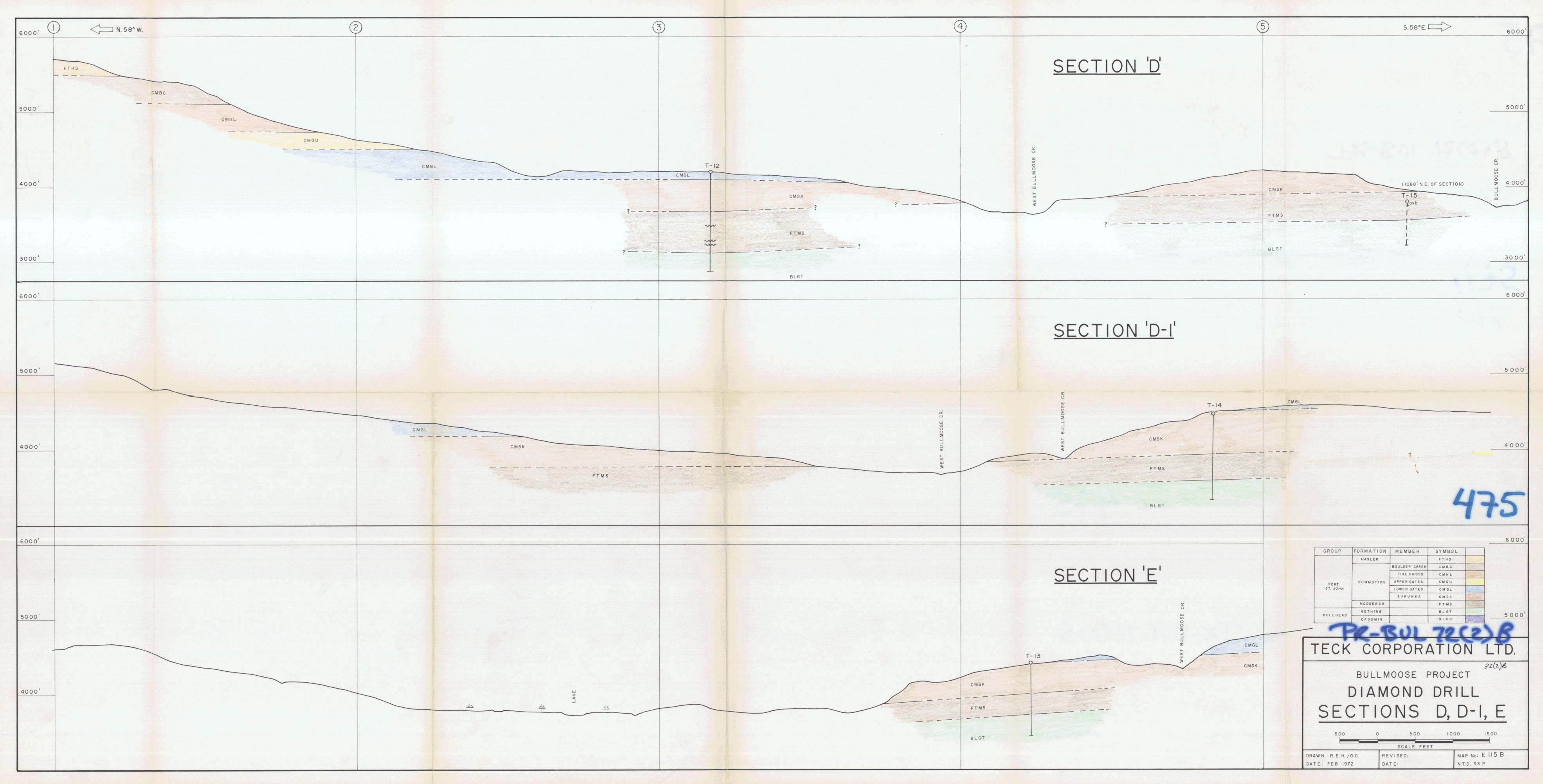
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SERIES	GROUP	FORMATION	MEMBER	OR SEAM	SEAMS	GROUPS FORMATIONS MEMBERS	
		HASLER				FTHS	
			BOUL DER CREEK			CMBC	
			HULCROSS			CMHL	
- 1	FORT	COMMOTION	UPPER GATES	UPPER GATES SEAMS I TO 8 INCL.	UGI - UGB INCL.	CMGU	
	ST. JOHN		LOWER GATES	LOWER GATES SEAMS 18 2	LGI & LG2	CMGL	316
			SUKUNKA			CMSK	5
-		MOOSEBAR				FTMS	
LOWER CRETACEOUS				BIRD SEAM UPPER MIDDLE LOWER SKEETER SEAM	BD UBD MBD LBD		
	BULLHEAD	GETHING		UPPER MIDDLE LOWER MID SEAMS	USK MSK LSK MS	BLGT	
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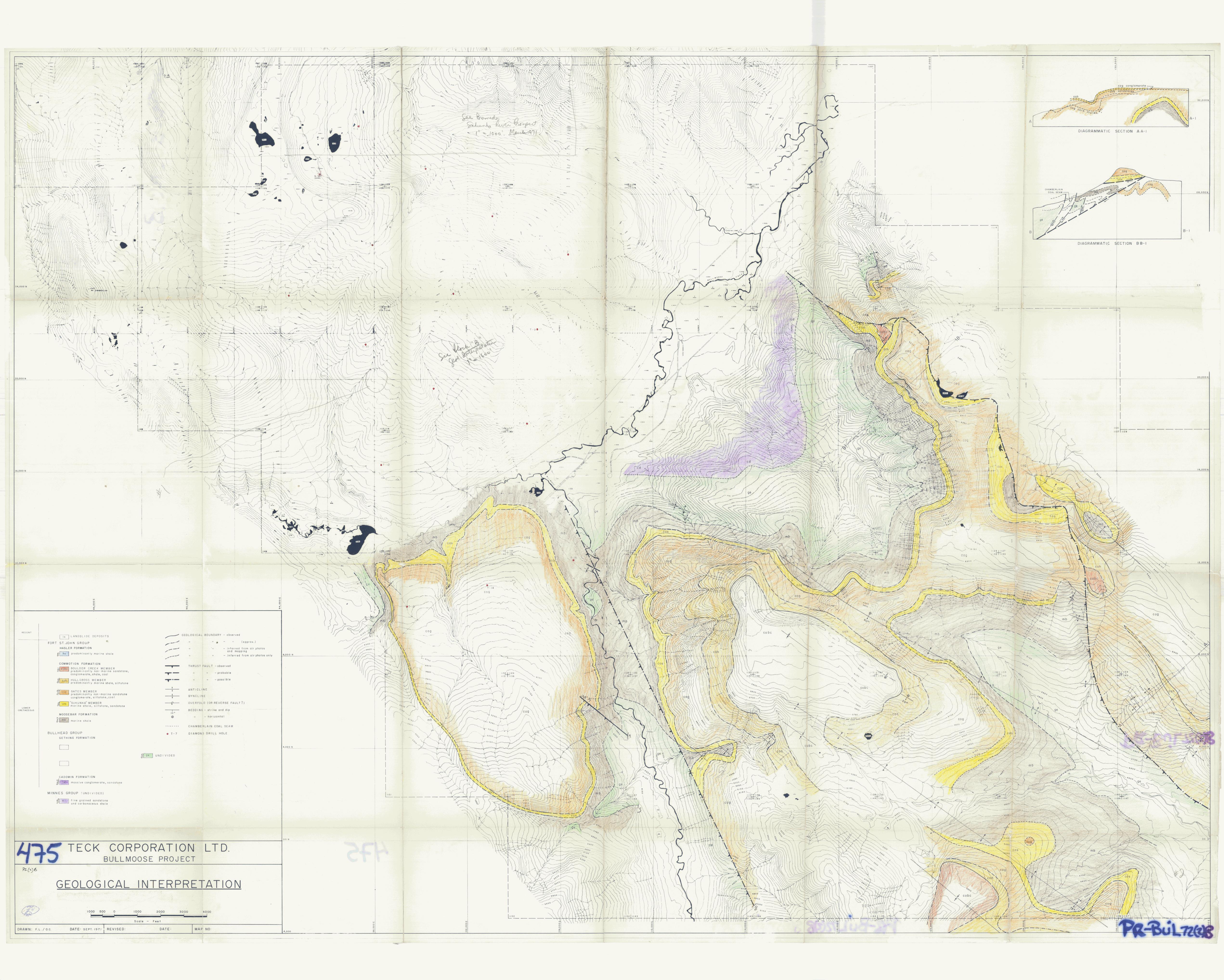


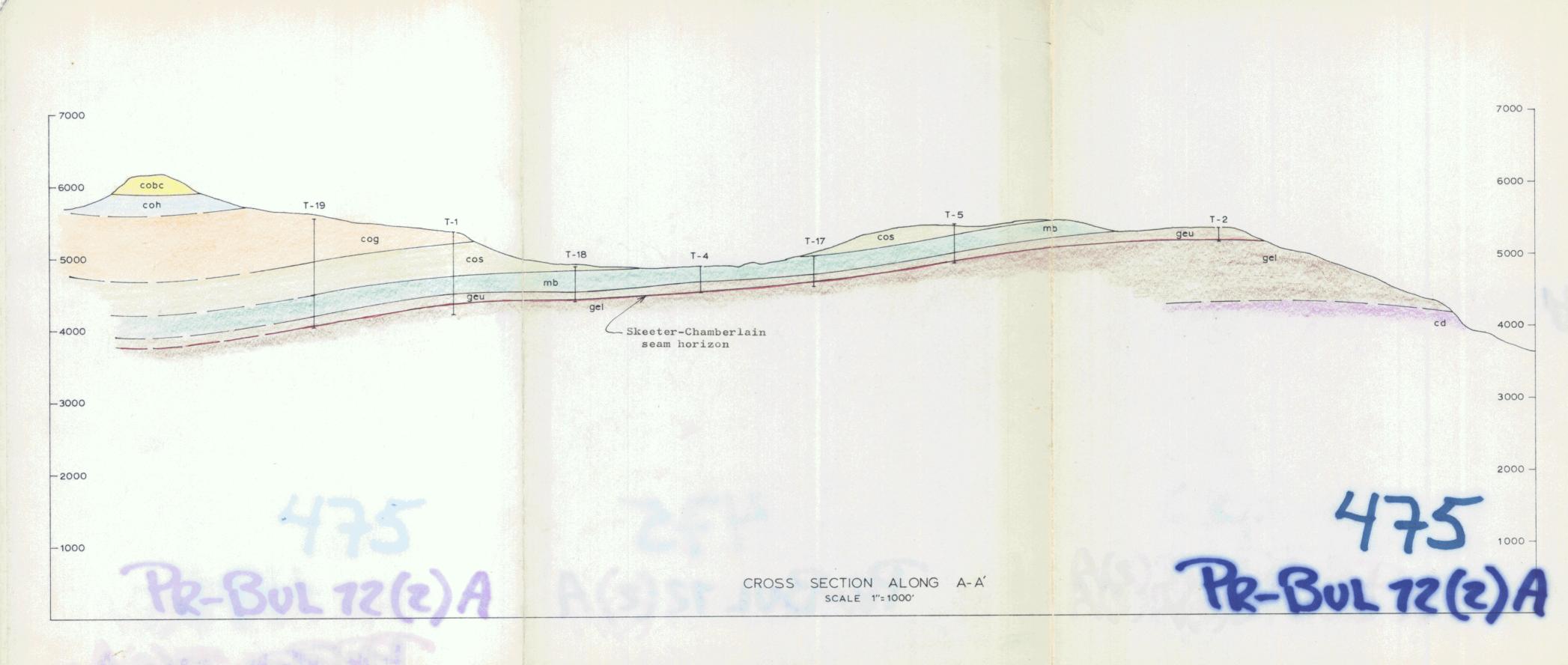


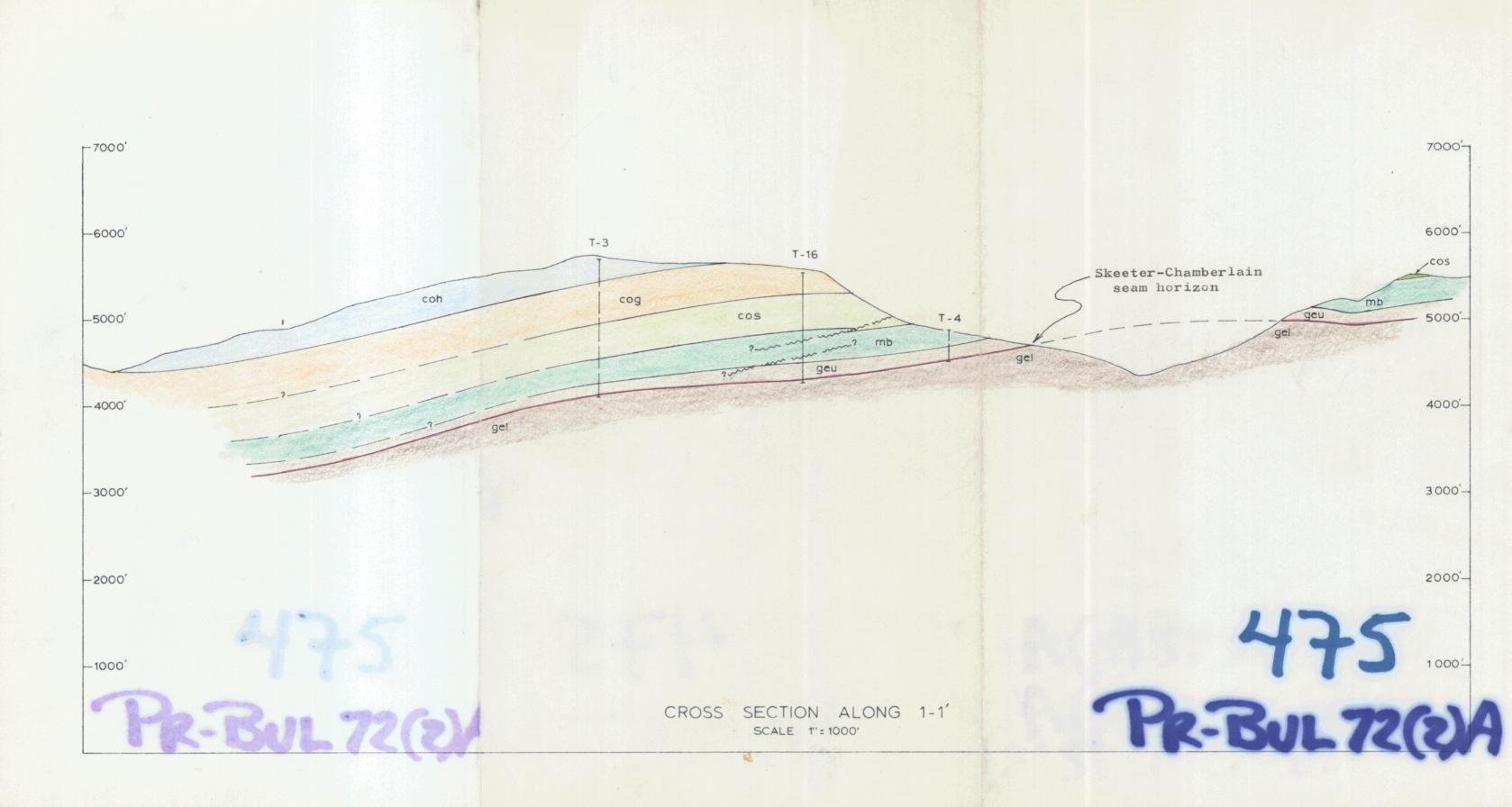


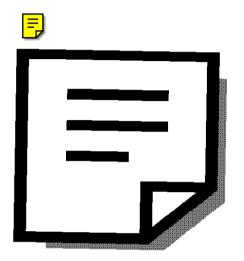












NOTE: COAL ANALYSIS DATA WAS TAKEN FROM OPEN 72(I)A PR-BULLMOOSE FILE

BULLMOUSE

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REPORT ON BULLMOOSE PROJECT, 1972

SUKUNKA RIVER AREA, B. C.

by

R. S. Verzosa

January 30, 1973

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Vancouver, B.C.

CONFIDENTIAL

APPENDIX I : COAL SAMPLE ANALYSES

CALLER STATE AND ANTE A SALE STALT, OHIGHGO HENOLS GUODE ANTA CODE 312 71-34944

Please address all correspondence to: 147 Riverside Drive, North Vancouver, S.C. U.N.C.C 1600

Office: Tel. (304) 925-2228 Roberts Bank Tel. (604) 946-7021

November 24, 1972

Teck Corporation Ltd., 700-1177 W. Hastings St., Vancouver, B. C.

Gentleman:

Enclosed are tabulated test results for coal cores from D.D.K. 1-6.

Following is the procedure for testing and the analysis.

- 1. Core was crushed to minus 3/4" sq.
- Crushed sample was subjected to float-sink cests at 1.35, 1.40, 1.45 and 1.55 specific gravities. Weight reporting to each gravity fraction was recorded.
- 3. Each gravity fraction was analyzed for ash and sulfur.
- The 1.35 float and the 1.40 float was analyzed for ash, volatile, fixed carbon, BTU, sulfur and free swelling index.
- 5. The plasticity index was determined for the raw coal from D.D.N. No.6.
- 6. Tabulations were made and charts were drawn to show the cumulative recovery and cumulative rejects.

Respectfully submitted, coldERCLAL TESTING & ENGINEERING CO. R. M. Houser, Dividion Memoger.

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COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 228 NORTH LA SALLE STREET, CHICAGO, ILLINOIS 80601 - AREA CODE 312 728-8434

Please address all correspondence to: 147 Riverside Drive, North Vancouver, B.C.



Office: Tel. (604) 929-2228 Roberts Bank Tel. (604) 946-7021

November 24, 1972

CERTIFICATE OF ANALYSIS FOR: Teck Corporation Ltd., 700 - 1177 W. Hastings St., Vancouver, B. C.

Sample Identification:

Report No. 67-3672

D.D.H. No. 6, Raw Coal.

COAL PLASTICITY (GIESELER PLASTCHETTR)

Maximum Fluidity, D.D.P.M.	22.0
Temp. at Maximum Fluidity, °C	465
Temp. at Initial Fluidity, °C	434
Temp. at Final Fluidity, °C	482
Range, °C	48
Torque - 40 gram inches	

Respectfully submitted,

COMMERCIAL TESTING & ENGINEERING CO.

122 A. Houser, R.

Division Manager.

RAH:dek



FUEL RESEARCH & INSTRUMENT COMPANY

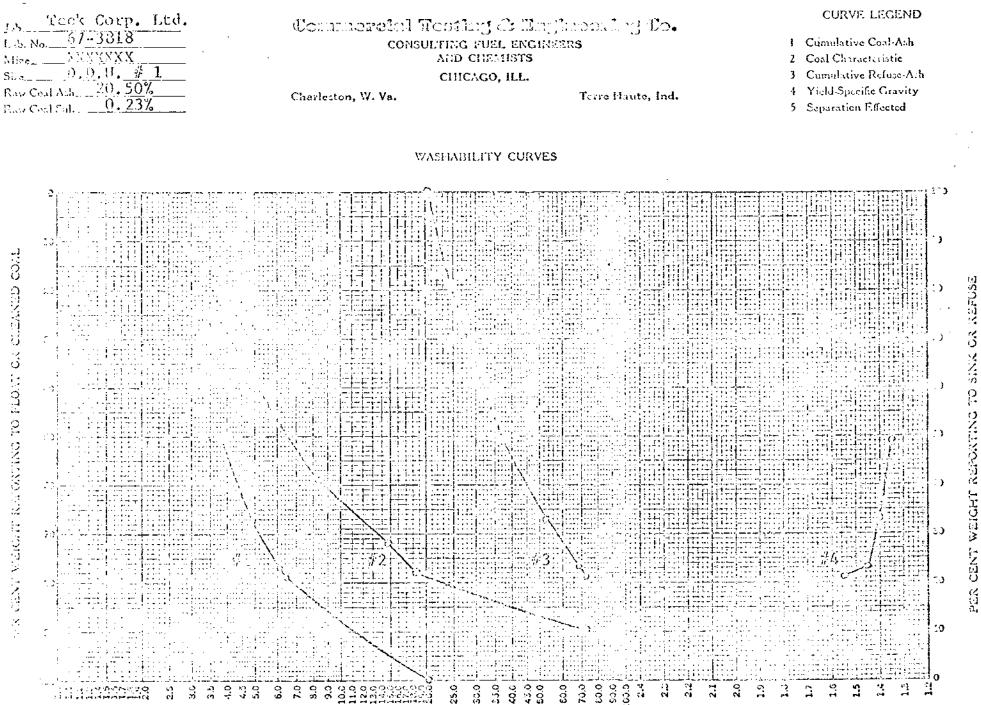
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VARCOUVER B.C., CANADA

Sample #1				FLOAT & SINK ANALYSIS				TESTED OCT. NOV. , 1972				
Specific <u>Gravity</u>			Raw Coal Crushed t		to 3/4" sq. x 0 Cumulative <u>Recovery</u>		···· L	Cumulative Reject		0		
007	Sink	<u>Float</u>	% Wt.	<u>% Ash</u>	% Sul.	<u>% Wt.</u>	<u>% Ash</u>	% Sul.	<u>% WE.</u>	% Ash	% Sul.	
AME		1.35	51.2	3.88	0.28	51.2	3.88	0.28	100.0	20.50	0,23	
COMMERCIAL	1.35	1.40	16.2	8.29	0.26	67.4	4.94	0.28	48.8	37,93	0,19	
		1.45	9.7	14.76	0.27	77.1	6.18	0.27	32.6	52.66	0.15	
TESTING	1.45	1,55	1.9	18.48	0.31	79.0	6.47	0.28	22.9	68,71	0,00	
1	1.55		21.0	73.26	0.08	100.0	20.50	0.23	21.0	73,26	0.03	
NGIN				PROXIMATE ANALYSIS								
& ENGINEERING		<u>1.35</u> Fl		oat = 51.1	2%	<u>1</u>	1.40 Float = 67.4%					
ING CO.		% Ash % Volatile % Fixed Carbon		3.88 19.41 76.71		4.94 19.20 <u>75.86</u>						
		BTU % Sulf	ur	14891 0.28			14661 0.28					
		FSI		1			1					



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Form WCR 3M 9-49

Copyright, 1939. Commercial Testing and Engineering Co.

ASH CONTENT IN PER CENT OF SAMPLE

SPECIFIC GRAVITY

VANCOUVER, B.C., CANADA

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ļ		Sample	#2	FLOAT & SINK ANALYSIS Raw Coal Crushed to 3/4" sq. x 0				TESTED OCTNOV., 1972				
	Specifi c Gravity		Dry Basis		Cumulative Recovery			Cumulative Reject				
	Sink Sink	Float	% Wt.	<u>% Ash</u>	<u>% Sul.</u>	<u>% Wt.</u>	% Ash.	<u>% Sul.</u>	% Wt.	<u>% Ash</u>	<u>% Sul.</u>	
	5 5 m	1.35	42.8	5,99	0.40	42.8	5.99	0.40	100.0	11.00	0.33	
	Constant Sink Sink 1.35	1.40	32.8	8.26	0.32	75.6	6.97	0.37	57.2	14.74	0,28	
	1. 40	1.45	16.6	14.30	0.29	92.2	8,29	0,35	24.4	23.46	0,26	
.	STIN 1.45	1.55	1.8	20.74	0.27	94.0	8.53	0.35	7.8	42,96	0,21	
	¢ 1.55		6.0	49.62	0.19	100.0	11.00	0.34	6.0	49.62	0.19	
	$\frac{PROXIMATE ANALYSIS}{1.35 \ Float = 42.8\%} \frac{1.40 \ Float = 75.6\%}{6.97}$											
	<u>1.35 F</u>			10at = 42.8%			.40 Float	= 75.6%				
	% Ash % Volatile % Fixed Carbon			5.99 18.76 <u>75.25</u> 100.00	-	6.97 18.31 74.72						
		BTU % Sulfu	ur	14542 0.40			100.00 14206 0.37					
		FSI		1			1					

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CORVE LEGEND

- AeA-IsoD svitriumD 1
- 2 Coal Characteristic
- AcA-seulasticiumu) &
- A Yield-Speedic Gravity
- Separation Effected

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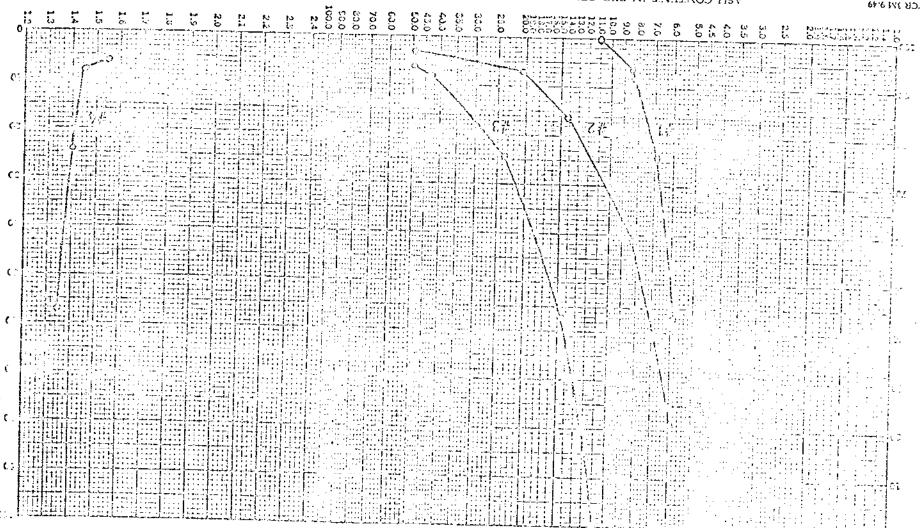
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Charleston, W. Vs.

BUN COLET U 37%
RAU Coal Ash 1.1.00%
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MASHARILLY CURVES

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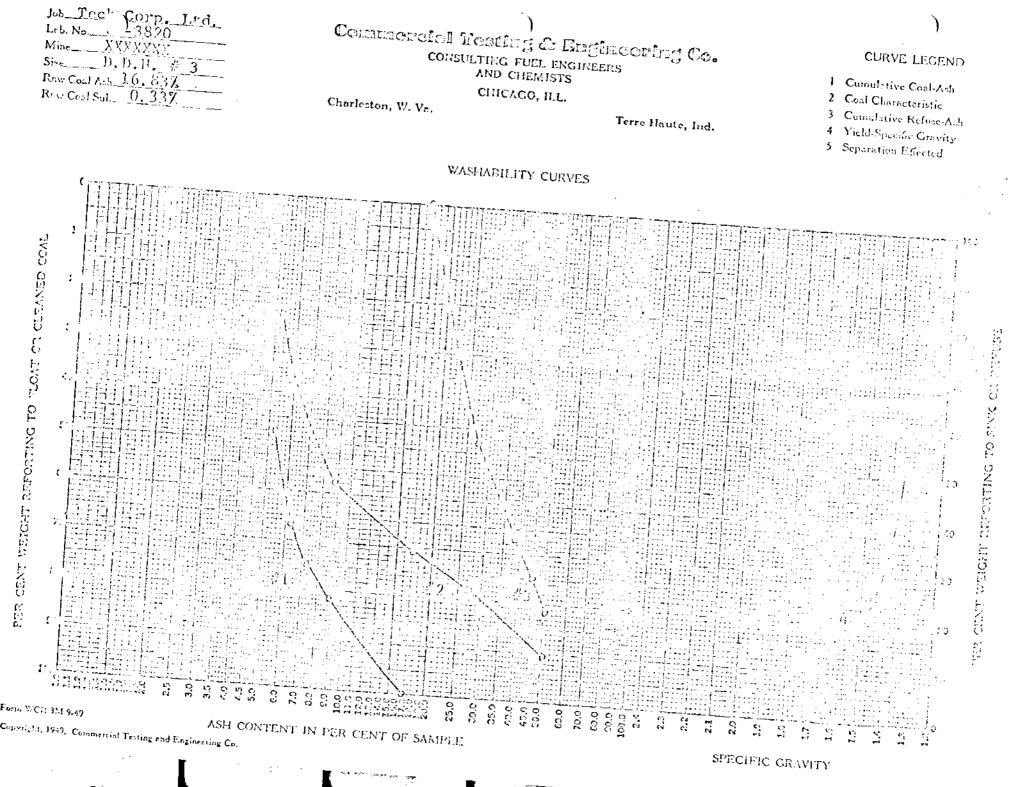
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VANCOUVER B.C., CANADA

	Sample #3			~	FLOAT & SINK ARALYSIS					TESTED OCTNOV., 1972		
	Raw Coal Crushed to $3/4"$ sq. x 0											
	Crow	Specific Gravity		Dry_Basis		Cumulative Recovery			Cumulative 			
	Sink	Float	% Wt.	% Ash	<u>% Sul.</u>	% Wt.	<u>% Ash</u>	<u>% Sul.</u>	% Wt.	<u>% Ash</u>	% Sul.	
	n 0)	1,35	48.0	5.26	0.37	48.0	5.26	0.37	100.0	16.83	0.33	
	1.35	1.40	19.3	8.82	0.35	67.3	6.28	0.36	52.0	27.51	0.30	
	1,40	1.45	7.6	17.08	0.36	74.9	7.38	0.36	32.7	38,54	0.27	
	1.45	1.55	6.6	27.14	0.35	81.5	8.97	0.36	25.1	45.04	0.25	
1			18.5	51,43	0.21	100.0	16.83	0.33	18.5	51.43	0.21	
	1				PROXIMA	TE ANALYS	15					
KIN			1.35 FI	oat = 48.(2%		1.40 F1	<u>oat = 67.</u>	.3%			
<u>6 CO.</u>	2 1.55 18.5 1.35 F1 2 C 2 K Ash % Volatile % Fixed Carbon			5.26 18.77 <u>75.97</u> 100.00				6.28 18.05 75.67 100.00				
		BTU % Sulfu	r	14630 0.37				14407 0.36				
		FSI		12				12				



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COMMERCIAL TESTING

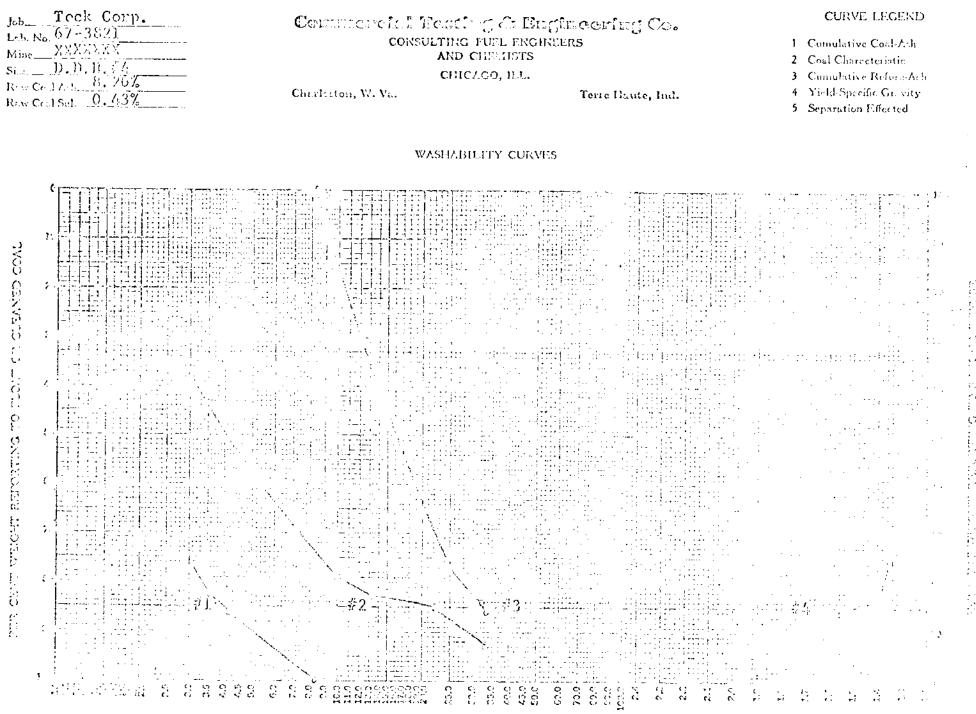
& ENGINEERING

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VARCOUVER, D. C., CANADA

	Sample	#4	FLOAT & STRK ANALYSIS TESTED OCENOV., 1972								
			Raw Cool	Crushed t	:o 3/4" so	. x 0				• • •	
-	cific vity_		Dry Basis			Cumulative Recovery			Cumulative Reject		
Sink	Float	<u>% Wt.</u>	<u>% Ash</u>	<u>% Sul.</u>	<u>% Wt.</u>	<u>% Ash</u>	<u>% Sul.</u>	<u>% Nt.</u>	% Ach	<u>% Sul.</u>	
	1,35	76.0	3.04	0.47	76.0	3.04	0.47	100.0	8,26	0,43	
1.35	1.40	6.6	9. 89	0.37	82.6	3.59	0.46	24.0	24.81	0.3)	
1.40	1.45	1.6	13.47	0.38	84.2	3.78	0.46	17.4	30.47	0.29	
n p 1,45	1.55	1.9	22,08	0.34	86.1	4.18	0.46	15.8	32.19	0.23	
1,55		13.9	33.57	0,27	100.0	8.26	0.43	13.9	33.57	0.27	
			PRO	MA ETANIXC	ALYSIS						
>		<u>1.35 F</u>	loat = 76.(6.0% 1.40 Floot = 82.6%							
)	% Ash % Volatile % Fixed Carbon		3.04 21.74 <u>75.22</u> 100.00		3.59 21.34 <u>75.07</u> 100.00						
	ETU % Sulfy	ur	15207 0.47		15013 0.46						
	FSI		9			8 ¹ 2		,			



For: MCR 3119.79

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VANCOUVER, B.C., CARADA

	Sample #5			FLOAT & STRE ARAINSIS TESTED OCT NOV., 3972							
				Raw Coal	Cruched t	<u>o 3/4" sc</u>	<u>. x 0</u>				
	~	ecific wity		Dry Ba	asis	C	umulative Recovery	······································	Cumulative Reject		
	COMMERCIAL TESTING	Float	<u>% Wt.</u>	% Ash	<u>% Sul.</u>	% Ht.	% Ash	<u>% Sul.</u>	% Wt.	% Ash	% Sul.
:	ERCI	1.35	58.3	3.72	0.35	58.3	3.72 ·	0.35	100.0	8.49	0.31
	1,35	1.40	16.3	9.46	0.27	74.6	4.97	0.33	41.7	15.16	0.26
	ST 1.40	1.45	17.7	13.34	0.27	92.3	6.58	0.32	25.4	18,83	0.25
	Շ թ.1.ՀՏ	3.55	3.9	21.27	0.25	96.2	7.17	0.32	7.7	31,44	0,25
	α 1,55		3.8	41.87	0.17	100.0	8.49	0.31	3.8	41.87	0.17
	M 1,55 QN 1,55 QN M R R N			PRO	XIMATE ANA	LYSIS					
	A NO		1.35F	<u>= 58,3%</u>		1,40) Float =	74.6%			
	0	% Ash % Volatile % Fixed Carbon		3.72 21.67 <u>74.61</u> 100.00			4.97 20.84 74.19 100.00				
		B1U % Sulfi	ur.	15099 0.35			14805 0.33				
		FSI		8			7				

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Containg weich Wootling & Engineers consulting fuel engineers and chemists chicago, ill.

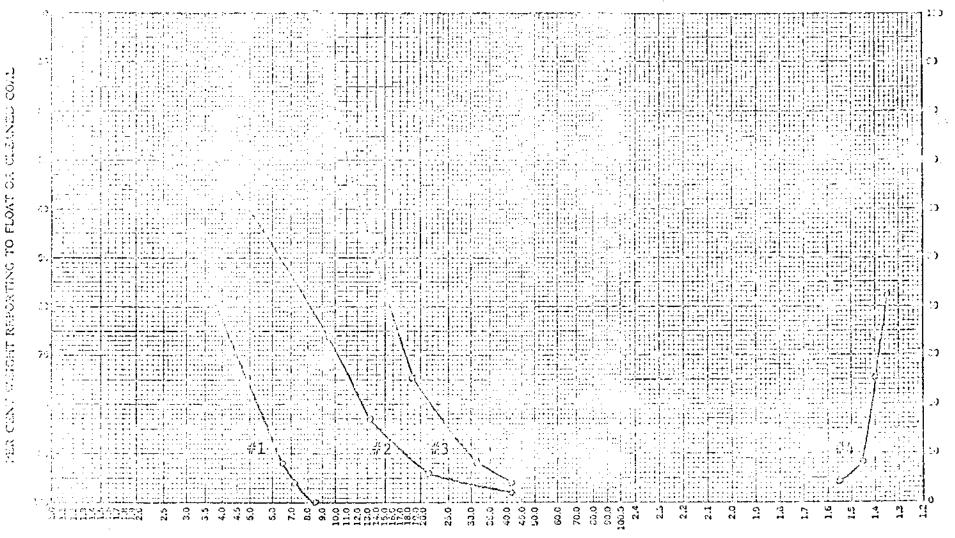
Terre Haute, Ind.

CURVE LEGEND

- 1 Cumulative Coal-Ach
- 2 Coal Characteristic
- 3 Cumulative Refuse-Ash
- 4 Yield-Specific Gravity
- 5 Separation Effected

Charleston, W. Va.

WASHABILITY CURVES



Form WCR 3M 9-49

ASH CONTENT IN PER CENT OF SAMPLE

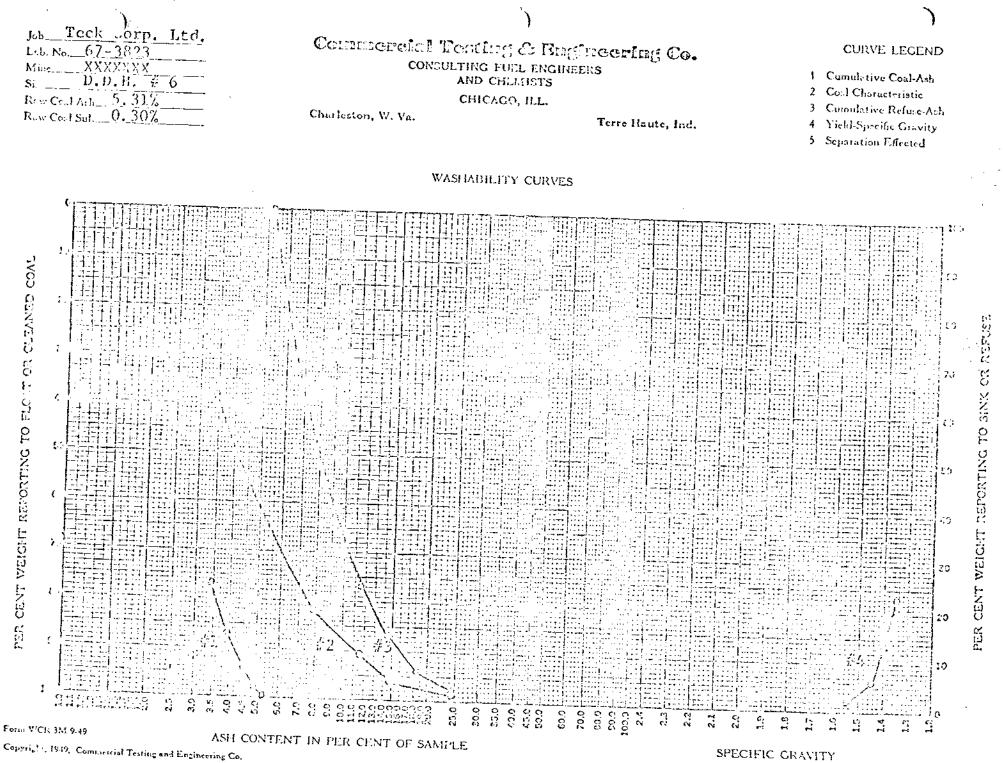
SPECIFIC GRAVITY

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VANCOUVER, B.C., CANADA

Sample #6 FLOAT & SURK ANALYSIS								TESTED OCT	<u>-NOV.</u>	<u>1972</u>	
Raw Coal Crushed to 3/4" sq. x								<u>)</u>			
	Specific <u>Gravity</u>		Dry Basis		Cumulative Recovery				Cumulative Reject	2	
COM	<u>Sink</u>	<u>Float</u>	<u>% Wt.</u>	% Ash	<u>% Sul.</u>	% Wt.	<u>% Ash</u>	<u>% Sul.</u>	<u>% Wt.</u>	<u>% As</u> h	<u>% Sul.</u>
COMMERCIAL		1.35	76.9	3.42	0.32	76.9	3.42	0.32	100.0	5.31	0.30
ALT	1.35	1.40	10.2	7.94	0.27	87.1	3,95	0.31	23.1	11.62	0.25
TESTING	1,40	1.45	7.1	11.48	0.26	94.2	4.52	0.31	12.9	14,53	0.24
G	1,45	1.55	3.7	14.79	0.22	97.9	4.91	0.31	5.8	18.27	0.27
			2.1	24.41	0.19	100.0	5.31	0.30	2.1	24.4 <u>1</u>	0.19
				PI	OXIMATE A	NALYSIS					
ENGINEERING CO		<u>1.3</u>		35F = 76.9%		1.40 Float = 87.1%					
CO.	% Ash % Volatile % Fixed Carbon			3.4221.5475.04100.00		3.9521.4374.62100.00					
		BTU % Sulfr	٩r	15072 0.32			14941 0.31				
		FSI		8			7				



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